

CORE STRUCTURE OF INTEGRAL HEAT-EXCHANGER

BACKGROUND OF THE INVENTION

1. Field of the Invention

5 The present invention relates to a core structure of an integral heat-exchanger in which corrugate fins of a first heat-exchanger and corrugate fins of a second heat-exchanger are integrally incorporated with one another.

10 Hitherto, there has been known, as disclosed in Laid-Open Japanese Patent Application No. 10-231724 or 11-294984, such a core structure of an integral heat-exchanger that corrugate fins of a first heat-exchanger and corrugate fins of a second heat-exchanger are integrally incorporated with one another.

15 In Fig. 18, there is shown a sectional view of a core structure of an integral heat-exchanger disclosed in the Laid-Open Japanese Patent Application 10-231724. It is to be noted that to assemble the heat-exchanger, a plurality of core structures are piled on one another. In each core structure, first heat-exchanger tubes 1 of a first heat-exchanger and second heat-exchanger tubes 2 of a second heat-exchanger are arranged front and back in two rows in an air-stream direction.

20 The first heat-exchanger is a condenser used to cool a refrigerant that flows in a circuit of an automotive air conditioner, and the second heat-exchanger is a radiator used for cooling an engine cooling water. A corrugated fin (wave-like fin) 3 is arranged between the first heat-exchanger tubes 1 and between the second heat-exchanger tubes 2. That is, the corrugated fin 3 includes a front corrugated part (no numeral) disposed between the first heat-exchanger tubes 1 and a rear corrugated part (no numeral) disposed between the second heat-exchanger tubes 2.

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The front and rear corrugated parts of the corrugated fin 3 are integrally incorporated with each other through the intermediary of a connection part 3a. Louvers 3b, 3c are formed

in the front and rear corrugated parts of the corrugated fin 3, as shown. Cut-out parts 3d and louvers 3e are formed in the connection part 3a.

Since the connection part 3a is formed therein with the cut-out parts 3d and the louvers 3e in this core structure, and the heat transfer through the corrugated fins 3 is obstructed by the cut-out parts 3d and the louvers 3e in the core part of this integral heat-exchanger, and accordingly, it is possible to restrain such thermal interference that heat is transferred, for example, from the higher temperature second heat-exchanger tubes 2 toward the lower temperature first heat-exchanger tubes 1 through the intermediary of the corrugated fins 3.

Referring to Fig. 19, there is shown a core structure of an integral heat-exchanger disclosed in Laid-Open Japanese Patent Application 11-294984. In this core structure, first heat-exchanger tubes 4 of a first heat-exchanger and second heat-exchanger tubes 5 are arranged front and back in two rows in an air stream direction. A corrugated fin (wave-like fin) 6 is arranged between the first heat-exchanger tubes 4 and between the second heat-exchanger tubes 5. That is, the corrugated fin 6 includes a front corrugated part (no numeral) disposed between the first heat-exchanger tubes 4 and a rear corrugated part (no numeral) disposed between the second heat-exchanger tubes 5.

The front and rear corrugated parts of the corrugated fin 6 are integrally incorporated with one another through the intermediary of a connection part 6a. Louvers 6b, 6c are formed in the front and rear corrugated parts of the corrugated fin 6, as shown. Also the connection part 6a is formed therein with louvers 6d.

In the core structure of this integral heat-exchanger, since the louvers 6d are formed in the connection part 6a, heat transfer through the corrugated fin 6 is obstructed, and accordingly, it is possible to restrain thermal interference such

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that heat is transferred, for example, from the higher temperature heat-exchanger tubes 5 toward the lower temperature second heat-exchanger tubes 4 through the corrugated fins 6.

5 However, in the core structures of the above-mentioned conventional integral heat-exchangers, due to provision of the cut-out parts 3d and louvers 6d in the connection parts 3a, 6a, heat entering into the connection part 3a, 6a is obstructed, and accordingly, there has been raised such a drawback that heat
10 radiation from the connection part 3a, 6a cannot be effectively made.

Further, if the louvers 3e, 6d are formed excessively in the connection part 3a, 6a, the air resistance becomes increased and thus makes the air flow poor, resulting in that the heat-exchanging performance is lowered.
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SUMMARY OF THE INVENTION

It is therefore an object of the present invention to provide a core structure of an integral heat-exchanger which is free the above-mentioned drawbacks

20 It is an object of the present invention is to provide a core structure of an integral heat-exchanger, which suppresses or at least minimizes thermal interference between the first heat-exchanger tubes and the second heat-exchanger tubes, and enhances the heat-radiating performance of the second heat-exchanger in the connection part.
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According to a first aspect of the present invention, there is provided a core structure of an integral heat-exchanger, which comprises at least two first heat exchanger tubes which extend in parallel with each other; at least two second heat exchanger
30 tubes which extend in parallel with each other, the two second heat exchanger tubes being juxtaposed with the two first heat exchanger tubes; and a corrugated fin including a corrugated first part interposed between the first heat exchanger tubes, a

corrugated second part interposed between the second heat exchanger tubes and a flat connection part arranged between the corrugated first and second parts, the corrugated first part of the fin being formed with a plurality of first louvers each

- 5 extending substantially between the two first heat exchanger tubes; the corrugated second part of the fin being formed with a plurality of second louvers each extending substantially between the two second heat exchanger tubes, the innermost one of the second louvers being positioned away from the innermost end of
- 10 the corrugated second part of the fin by a given length; and the flat connection part being formed with a third louver in the vicinity of the innermost one of said first louvers, the third louver being constructed to obstruct a heat transfer in the fin.

According to a second aspect of the present invention,

- 15 there is provided a core structure of an integral heat-exchanger, which comprises at least two first heat exchanger tubes which extend in parallel with each other; at least two second heat exchanger tubes which extend in parallel with each other, the second heat exchanger tubes being juxtaposed with the first
- 20 heat exchanger tubes; and a corrugated fin including a corrugated first part interposed between the first heat exchanger tubes, a corrugated second part interposed between the second heat exchanger tubes and a flat connection part arranged between the corrugated first and second parts, the corrugated
- 25 first part of the fin being formed with a plurality of first louvers each extending substantially between the two first heat exchanger tubes; the corrugated second part of the fin being formed with a plurality of second louvers each extending substantially between the two second heat exchanger tubes; and
- 30 the flat connection part being formed with a plurality of heat radiation portions, each radiation portion being constructed not to largely deteriorate the heat transfer in the fin.

BRIEF DESCRIPTION OF THE DRAWINGS

Other objects and advantages of the present invention will become apparent from the following description when taken in conjunction with the accompanying drawings, in which:

5  Fig. 1 is a perspective view of an integral heat-exchange having a core structure according to the present invention;

10 Fig. 2 is a sectional view of a part of core structure of an integral heat-exchanger, which is a first embodiment of the present invention;

15 Fig. 3 is a graph showing a relation between the length of a corrugated fin and a local heat transfer;

Fig. 4 is a view similar to Fig. 2, but showing a second embodiment of the present invention;

Fig. 5 is a view similar to Fig. 4, but showing a basic arrangement of a core structure;

Fig. 6 is a view similar to Fig. 2, but showing a third embodiment of the present invention;

Fig. 7 is a view similar to Fig. 2, but showing a fourth embodiment of the present invention;

20 Fig. 8 is a view similar to Fig. 2, but showing a fifth embodiment of the present invention;

Fig. 9 is a view similar to Fig. 2, but showing a sixth embodiment of the present invention;

Fig. 10 is a view similar to Fig. 2, but showing a seventh embodiment of the present invention;

25 Fig. 11 is a view similar to Fig. 2, but showing an eighth embodiment of the present invention;

Fig. 12 is a view similar to Fig. 2, but showing a ninth embodiment of the present invention;

30 Fig. 13 is a view similar to Fig. 2, but showing a tenth embodiment of the present invention;

Fig. 14 is a view similar to Fig. 2, but showing an eleventh embodiment of the present invention;

Fig. 15 is a view similar to Fig. 2, but showing a twelfth embodiment of the present invention;

Fig. 16 is a view similar to Fig. 2, but showing a thirteenth embodiment of the present invention;

5 Fig. 17 is a view similar to Fig. 2, but showing a fourteenth embodiment of the present invention;

Fig. 18 is a view similar to Fig. 2, but showing a first known core structure of an integral heat-exchanger; and

10 Fig. 19 is a view similar to Fig. 2, but showing a second known core structure of an integral heat-exchanger.

DETAILED DESCRIPTION OF THE EMBODIMENTS

In the following, detailed explanation of the present invention will be made with reference to the accompanying drawings. Throughout the specification, substantially same parts and portions are denoted by the same reference numerals.

15 Fig. 1 shows an integral heat-exchanger having a core structure according to the present invention. The integral heat-exchanger generally comprises first and second twin tank portions T1 and T2. Each tank portion T1 or T2 is divided into

20 front and rear tanks. Between the first and second twin tank portions T1 and T2, there extend a plurality of core structures CS which are piled on one another. As will become apparent as the description proceeds, the core structures CS include a front part that is incorporated with the front tanks of the tank portions T1 and T2 to constitute a condenser and a rear part that is incorporated with the rear tanks of the tank portions T1 and T2 to constitute a radiator.

25 In the following, various embodiments of the present invention will be described with reference to Figs. 2 to 17. In these drawings except Fig. 3, all of the core structures of these embodiments are arranged to permit air to flow from the left side toward the right side.

30 Fig. 2 shows a first embodiment of a core structure of an

integral heat-exchanger according to the present invention.

In the core structure of this integral heat-exchanger, a corrugated fin 15 of aluminum is arranged between first heat-exchanger tubes 11 of a first heat-exchanger and between second heat-exchanger tubes 13 of a second heat-exchanger.

5 The first heat-exchanger may be a condenser used to cool a refrigerant that flows in a circuit of an automotive air conditioner, and the second heat-exchanger may be a radiator used for cooling an engine cooling water. The corrugated fin 15 includes

10 a front corrugated part (no numeral) disposed between the first heat-exchanger tubes 11 through welded portions and a rear corrugated part (no numeral) disposed between the second heat-exchanger tubes 13 through welded portions. It is to be noted that to assemble the integral heat-exchanger, a plurality of core

15 structures are piled on one another. It is further to be noted that upon assembly on a motor vehicle, the first heat-exchanger is arranged on the upstream side while the second heat-exchanger is arranged on the downstream side, with respect to the flow of air.

20 The first heat-exchanger tubes 11 and the second heat-exchanger tubes 13 are formed of flattened tubes made of aluminum plate or the like. Each tube 11 or 13 is formed with rounded front and rear ends 11a, 13a, as shown. The thickness of each tube 11 or 13 is about 1.7 mm, and each tube 11 or 13

25 is formed at lower and upper surfaces thereof with flat joint portions 11b, 13b. Each of these flat joint portions 11b, 13b is connected to crest portions of the corresponding corrugated fin 15 by brazing. That is, the lower surface of each tube 11 or 13 is brazed to upper crest portions of a fin 15 that is positioned

30 below the tube 11 or 13, and the upper surface of each tube 11 or 13 is brazed to lower crest portions of another fin 15 that is positioned above the tube 11 or 13.

In this first embodiment, the corrugated fin 15 has a first

joint zone 15a where the joint portions 11b of the first heat-exchanger tubes 11 are located. In this first joint zone 15a, a plurality of function enhancing louvers 15c are successively formed at a given pitch of, for example, 1 mm. Further, a single
5 heat transfer preventing louver 15e is formed at a position inside of the inner end 15d of the first joint zone 15a, subsequent to the function enhancing louvers 15c, at a pitch equal to the pitch of the latter.

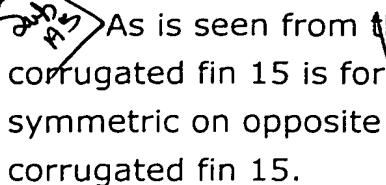
~~Sub P1H~~ The corrugated fin 15 also has a second joint zone 15b
10 where the joint portions 13b of the second heat-exchanger tubes 13 are located. In this second joint zone 15b, a plurality of function enhancing louvers 15h are successively formed in a portion which excepts such a zone that is extended by a predetermined distance X from the inner end 15f of the second
15 joint zone 15b.

It is noted that the predetermined distance X is greater than the pitch of the louvers, but preferably less than 2 mm, that is, it is desirably set to 1 mm although it is dependent upon the length L2 of the flat heat transfer part which will be explained
20 later.

A smooth flat connection part 15j is provided which is free from louvers, cutout parts and the like, in the corrugated fin 15 between the heat transfer preventing louver 15e and the function enhancing louvers 15h in the second joint zone 15b. It
25 is noted that the flat connection part 15j includes a part which serves as a single louver. The length L2 of a flat heat transfer part 15n which continuously extends from the second joint zone 15b up to the heat transfer preventing louver 15e is less than 12 mm, preferably less than 8 mm.

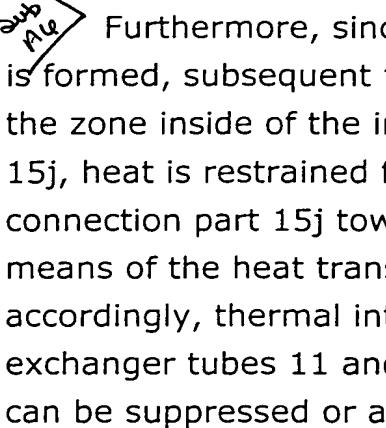
30 It is noted that there are formed, in this embodiment, a first flat part 15k and a second flat part 15m in which no louvers other than the single louver in the inner end part are formed, outside of the first joint zone 15a and second joint zone 15b of

the corrugated fin 15.

 As is seen from the lower illustration of Fig. 2, the corrugated fin 15 is formed with louvers 15c, 15e, 15d which are symmetric on opposite sides of the center line C of the corrugated fin 15.

5 In the core structure of the integral heat-exchanger, the function enhancing louvers 15h are successively formed in the second joint zone 15b, except the part which extends in the predetermined distance X from the inner end 15f of the second 10 joint zone 15b, and accordingly, heat from the second heat-exchanger tubes 13 is surely transferred from the zone which extends in the predetermined distance X from the inner end 15f of the second joint zone 15b, to the flat connection part 15j.

15 Heat led to the flat connection part 15j is effectively radiated into the open air passing by the corrugated fin 15, in the flat connection part 15j.

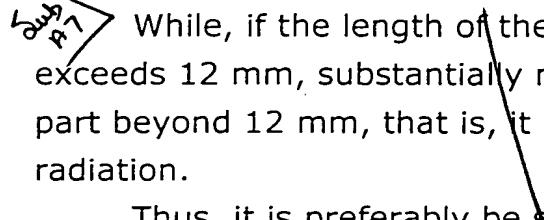
 Furthermore, since the heat transfer preventing louver 15e is formed, subsequent to the function enhancing louvers 15c, in the zone inside of the inner end 15d of the flat connection part 20 15j, heat is restrained from being transferred from the flat connection part 15j toward the first heat-exchanger tubes 11, by means of the heat transfer preventing louver 15e, and accordingly, thermal interference between the first heat-exchanger tubes 11 and the second heat-exchanger tubes 13 25 can be suppressed or at least minimized.

That is, in the core structure of the integral heat-exchanger as mentioned above, since the heat transfer preventing louver 15e is formed, subsequent to the function enhancing louvers 15c, in the zone inside of the inner end 15d of 30 the first joint zone 15a while the function enhancing louvers 15h are successively formed in the second joint zone 15b, except the part extending in the predetermined distance X from the inner end 15f of the second joint zone 15b, and since the flat

connection part 15j is formed between the heat transfer preventing louver 15e and the function enhancing louvers 15h in the second joint zone 15b, the heat interference between the first heat-exchanger tubes 11 and the second heat-exchanger tubes 13 can be reduced, and the function of heat radiation of the second heat-exchanger can be enhanced in the flat connection part 15.

Further, in the core structure of the integral heat-exchanger, as mentioned above, since the length L_2 of the flat heat transfer part 15n is less than 12 mm, and since the predetermined distance X is greater than the pitch of the louvers, the heat radiation can be effectively made in the flat connection part 15j.

That is, should the predetermined distance X be less than the pitch of the louvers, heat with which the flat connection part 15j can be sufficiently used, could not be transferred. However, should the predetermined distance X exceed 2 mm, the heat-exchanging function of the function enhancing louvers 15h would be deteriorated. Thus, it is preferable to set the predetermined distance X to be less than 2 mm.

 While, if the length of the flat heat transfer part 15n exceeds 12 mm, substantially no heat transfer is effected in the part beyond 12 mm, that is, it does not contribute to heat radiation.

Thus, it is preferably be set to a value less than 8 mm.

Referring to Fig. 3, there is shown a graph which shows a relationship between the local heat transfer Q_L of the corrugated fin 15 and the length L_2 of the flat heat transfer part 15n, which was obtained through simulation analysis on the basis of a basic formula for the function of a heat-exchanger. From this graph, it is found that substantially no heat transfer occurs in a part where the length L_2 of the flat heat transfer part exceeds 12 mm.

The above-mentioned basic formula is exhibited by:

$$Q_L = a_L A (T_{fl} - T_{aL}) \dots \dots \dots (1)$$

where Q_L is the local heat transfer, a_L is a local heat transfer coefficient, A is a local heat radiation area, T_{fl} is a fin temperature, and T_{aL} is an air temperature.

5 . . . In the core structure of the integral heat-exchanger as mentioned above, louvers 15c, 15e, 15d are symmetrically formed on the opposite sides of the center line C of the corrugated fin 15, and accordingly, the corrugated fin 15 can be surely manufactured in a well-balanced manner. Furthermore, a

10 10 single heat transfer preventing louver 15e is formed in the zone inside of the inner end 15d of the first joint zone 15a, and accordingly, the length L1 of the flat connection part 15j can be sufficiently ensured, thereby it is possible to surely carry out heat transfer.

15 It is noted that although the explanation has been made of such an embodiment that the single heat transfer preventing louver 15e is formed in the zone inside of the inner end 15d of the first joint zone 15a, the present invention should not be limited to this embodiment. That is, a plurality of heat transfer preventing louvers may be provided.

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Referring to Fig. 4, there is shown a second embodiment of the present invention. In this embodiment, the external dimensions of the first heat-exchanger tubes 11 are equal to that of the second heat-exchanger tubes 13, and the length of the

25 first joint zone 15a is equal to that of the second joint zone 15b. The length L1 of the flat joint part 15j is equal to the length L3 between the joint zones. Furthermore, the louvers 15c, 15e, 15h of the corrugated fin 15 in the air flow direction are symmetrically formed on opposite sides of the center line C of

30 the corrugated fin 15. Furthermore, all louvers 15c, 15e, 15d are arranged at a constant pitch P.

In this core structure of this second embodiment, since the length of the flat connection part 15j is equal to the length

between the joint zones, the heat transfer preventing louver 15e and the predetermined distance X can be easily provided by shifting the configuration of the corrugated fin 15 from the basic configuration thereof. That is, in the basic configuration shown

5 in Fig. 5, the center line C of the corrugated fin 15 is located at the center position between the first heat-exchanger tubes 11 and the second heat-exchanger tubes 13, and the function enhancing louvers 15c, 15h are successively formed in the first joint zone 15a and the second joint zone 15b. Furthermore, the

10 function enhancing louvers 15c, 15h are formed at positions which correspond to the inner end 15d of the first joint zone 15a and the inner end 15f of the second joint zone 15b. Accordingly, by shifting the center line C of the corrugated fin 15 from this basic configuration by one pitch P toward the second heat-

15 exchanger tubes 13, that is, toward the downstream side with respect to the air flow direction, as shown in Fig. 4, there can be easily obtained such a core structure that the heat transfer preventing louver 15e is formed on the fin 15 at the side of the first heat-exchanger tubes 11 while the predetermined distance

20 X is provided on the fin 15 at the side of the second heat-exchanger tubes 13.

Referring to Fig. 6, there is shown a third embodiment of the present invention. The core structure of this third embodiment is substantially the same as that of the above-mentioned second embodiment of Fig. 4 except the arrangement of the first and second heat-exchanger tubes 11 and 13 with respect to the air flow direction. That is, in the third embodiment, the second heat-exchanger tubes 13 are arranged at an upstream side and the first heat-exchanger tubes 11 are arranged at a downstream side, as shown in Fig. 6. In this arrangement, the heat transfer preventing louver 15e is provided in the vicinity of the second heat-exchanger tubes 13 for the radiator. Thus, undesired thermal interference from the higher

temperature side, viz., the second heat-exchanger tubes 13 to the lower temperature side, viz., the first heat-exchanger tubes 11 is suppressed. Furthermore, in this third embodiment, the heat radiation effect of the lower temperature side heat

5 exchanger (viz., first heat exchanger or the condenser) can be enhanced.

Referring to Fig. 7, there is shown a fourth embodiment of the present invention. This embodiment has such a configuration that the length of the first joint zone 15a for the

10 first heat-exchanger tubes 11 is equal to that of the second joint zone 15b for the second heat-exchanger tubes 13.

The louvers 15c, 15e, 15h of the corrugated fin 15 are symmetrically formed on the opposite sides of the flat connection part 15j, and a first flat part 15k and a second flat part 15m in which no louvers are formed are obtained on both sides of the corrugated fin 15. Furthermore, the first flat part 15k and the second flat part 15m have different lengths L4, L5, respectively, and the first flat part 15k and the second flat part 15m are projected from the first joint zone 15a and the second joint zone 15b, respectively, by an equal length L6. Further, in this fourth embodiment, the first heat transfer preventing louver 15e is formed on the fin 15 at the side of the first heat-exchanger tubes 11, and the length L4 of the first flat part 15k is longer than the length L5 of the second flat part 15m.

25 In the core structure of this embodiment, since the louvers 15c, 15e, 15d of the corrugated fin 15 are symmetrically formed on the opposite sides of flat connection part 15j, deformation of the corrugated fin which is likely to occur during processing of the corrugated fin 15 can be suppressed. Further, since the

30 lengths of the first flat part 15k and the second flat part 15m are different from each other, and since they are projected from the first joint zone 15a and the second joint zone 15b, respectively, by an equal length L6, the corrugated fin 15 can be arranged in a

well-balanced manner between the first heat-exchanger tubes 11 and the second heat-exchanger tubes 13.

Referring to Fig. 8, there is shown a fifth embodiment of the present invention. The core structure of this fifth embodiment is substantially the same as that of the above-mentioned fourth embodiment of Fig. 7 except the arrangement of the first and second heat-exchanger tubes 11 and 13 with respect to the air flow direction. That is, in this fifth embodiment, the second and first heat-exchanger tubes 13 and 11 are arranged at upstream and downstream sides respectively, as shown in Fig. 8.

In this fifth embodiment, advantages substantially equal to those of the above-mentioned fourth embodiment can be obtained.

Referring to Fig. 9, there is shown a sixth embodiment of the present invention. The core structure of this embodiment is substantially the same as that of the above-mentioned first embodiment of Fig. 2 except the arrangement of the first and second heat-exchanger tubes 11 and 13.

As shown, the heat transfer preventing louver 15e is formed on the fin 15 at the side of the first heat-exchanger tubes 11.

In the core structure of this fifth embodiment, the louvers 15c, 15d, 15h of the corrugated fin 15 are symmetrically formed on the opposite sides of the center line C of the corrugated fin 15, and accordingly, undesired deformation of the corrugated fin 15, which tends to appear during processing thereof, can be suppressed or at least minimized. Furthermore, since the width of the first heat-exchanger tubes 11 is different from that of the second heat-exchanger tubes 13, and since the first flat part 15k and the second flat part 15m are projected respectively from the first joint zone 15a and the second joint zone 15b by an equal length, the corrugated fin 15 can be arranged between the first

heat-exchanger tubes 11 and the second heat-exchanger tubes 13 in a well-balanced manner.

Referring to Fig. 10, there is shown a seventh embodiment of the present invention. In this embodiment, the length of the 5 first joint zone 15a for the first heat-exchanger tubes 11 is equal to that of the second joint zone 15b for the second heat-exchanger tubes 13. The numbers of the louvers 15c, 15e, 15h of the corrugated fin 15 are different from each other on the opposite sides of the flat connection part 15j. That is, in this 10 seventh embodiment, the number of the louvers on the fin 15 at the side of the first heat-exchanger tubes 11 is greater than that on the side of the second heat-exchanger tubes 13 by one, and the heat transfer preventing louver 15e is formed on the fin 15 at the upstream side with respect to the air flow direction, that is, 15 at the side of the first heat-exchanger tubes 11. Furthermore, the length L7 of the first flat part 15k is equal to that of the second flat part 15m, and the first flat part 15k and the second flat part 15m are projected respectively from the first joint zone 15a and the second joint zone 15m by an equal length L6.

20 In the core structure in this seventh embodiment, since the numbers of the louvers 15c, 15e, 15h of the corrugated fin 15 in the air flow direction are different from each other on the opposite sides of the flat connection part 15j, and since the first flat part 15k and the second flat part 15m are projected 25 respectively from the first joint zone 15a and the second joint zone 15m by an equal length, the corrugated fin 15 can be arranged in an well-balanced manner between the first heat-exchanger tubes 11 and the second heat-exchanger tubes 13.

Referring to Fig. 11, there is shown an eighth embodiment 30 of the present invention. The core structure of this embodiment is substantially the same as that of the above-mentioned seventh embodiment of Fig. 10 except the arrangement of the first and second heat-exchanger tubes 11 and 13. In this eighth

embodiment, the heat transfer preventing louver 15e is formed on the fin 15 at the downstream side with respect to the air flow direction, that is, at the side of the first heat-exchanger tubes 11, and first flat part 15k and the second flat part 15m are projected 5 respectively from the first joint zone 15a and the second joint zone 15b by an equal length L6.

In this eighth embodiment, substantially same advantages as those of the seventh embodiment can be obtained.

Referring to Fig. 12, there is shown a ninth embodiment of 10 the present invention. In this ninth embodiment, the flat connection part 15j is formed therewith a plurality of heat radiation parts for radiating heat without greatly hindering heat transfer from the second heat-exchanger tubes 13. In this ninth embodiment, the heat radiation parts are auxiliary heat radiation 15 louvers 21 having a length shorter than that of the function enhancing louvers 15c, 15h and the heat transfer preventing louver 15e.

In this ninth embodiment, heat from the second heat-exchanger tubes 13 is transferred to the flat connection part 15j 20 without being greatly hindered by the auxiliary heat radiation louvers 21, and accordingly, the heat is efficiently radiated from the plurality of auxiliary heat radiation louvers 21.

Furthermore, in this ninth embodiment, since the heat radiation parts are the auxiliary heat radiation louvers 21 having 25 a length which is shorter than that of the function enhancing louvers 15c, 15h and the heat transfer preventing louver 15e, the function of heat radiation is enhanced without hindering the heat transfer through the flat connection part 15j, and thermal interference between the first heat-exchanger tubes 11 and the 30 second heat-exchanger tubes 13 can be suppressed or at least minimized.

Referring to Fig. 13, there is shown a tenth embodiment of the present invention. In this embodiment, a plurality of

auxiliary heat radiation louvers 23 constituting a heat radiation part are arranged at certain intervals in a direction perpendicular to the air flow direction.

In this tenth embodiment, since the auxiliary heat radiation louvers 23 are arranged at certain intervals in a direction perpendicular to the air flow direction, the function of heat radiation can be enhanced.

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Referring to Fig. 14, there is shown an eleventh embodiment of the present invention. In this embodiment, the 10 heat radiation part has projections 25 formed in the flat connection part 15j. The projections 25 are formed in a pyramid shape.

In this eleventh embodiment, since the heat radiation part is composed of the projections 25 integrally incorporated with 15 the flat connection part 15j, the function of heat radiation can be enhanced without hindering heat radiation through the flat connection part 15j.

It is to be noted that the shape of each of the projections 25 may be formed in a conical shape or a trigonal pyramid.

20 Referring to Fig. 15, there is shown a twelfth embodiment of the present invention. In this embodiment, the heat radiation part has raised parts 27 formed by cutting and raising the flat connection part 15j. These raised parts 27 are formed in a triangular shape.

25 In this embodiment, since the heat radiation part is composed of the raised parts 27 formed by cutting and raising the flat connection part 15j, the function of heat radiation can be enhanced without greatly hindering heat transfer through the flat connection part 15j.

30 Each of the raised parts 27 may be formed in a rectangular shaped or the like.

Referring to Fig. 16, there is shown a thirteenth embodiment of the present invention. In this embodiment, the

length of the first joint zone 15a is equal to that of the second joint zone 15b. Furthermore, in this thirteenth embodiment, the number of the function enhancing louvers 15c on the first joint zone 15a and the heat transfer preventing louver 15e is 15 in total, and the number of the function enhancing louvers 15h on the second joint zone 15b is 14 in total. That is, in a zone that extends from the center line C toward a front end of the first joint zone 15a, there are provided fifteen louvers, while in a zone that extends from the center line C toward a rear end of the second joint zone 15b, there are provided 14 louvers.

Furthermore, all louvers 15c, 15h and 15e are arranged at a constant pitch. On the flat connection part 15j, there are formed two pyramid-shaped projections 25. As shown, the projections 25 are located closer to the second joint zone 15b by a distance L5 from the center line C.

In this thirteenth embodiment, since the heat radiation projections 25 are located closer to the second joint zone 15b which has less louvers than the first joint zone 15a, undesired deformation of the corrugated fin 15, which tends to appear during processing thereof, can be suppressed or at least minimized. Laid-Open Japanese Patent Application 2000-220983 describes the deformation of a fin which occurs during the processing.

Referring to Fig. 17, there is shown a fourteenth embodiment of the present invention. In this embodiment, the distance L8 between the heat transfer preventing louver 15e and its closest function enhancing louver 15c of the first joint zone 15a is greater than the distance L9 between the two adjacent function enhancing louvers 15c.

Due to this arrangement, the heat transfer preventing louver 15e can be assuredly located inside of the inner end 15d of the first joint zone 15a. That is, during processing of the corrugated fin 15, it tends to occur that the heat transfer

preventing louver 15e is produced at a position away from a desired position, or during assembling process, it tends to occur that the heat transfer preventing louver 15e is positioned away from a desired position with respect to the first and second heat-exchanger tubes 11 and 13. However, in this fourteenth embodiment, since, as is described hereinabove, the distance L8 between the heat transfer preventing louver 15e and its closest function enhancing louver 15c of the first joint zone 15a is greater than the distance L9 between the two adjacent function enhancing louvers 15c, the heat transfer preventing louver 15e can be assuredly located inside of the inner end 15d of the first joint zone 15a.

Although the invention has been described above with reference to the embodiments of the invention, the invention is not limited to such embodiments as described above. Various modifications and variations of such embodiments may be carried out by those skilled in the art, in light of the above descriptions.